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10/662,969	09/15/2003	Trevor MacDougall	WEAT/0414	1106

  

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EXAMINER	
LIU, LI	

  

ART UNIT	PAPER NUMBER
2613	

  

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**Please find below and/or attached an Office communication concerning this application or proceeding.**

The time period for reply, if any, is set in the attached communication.

**Office Action Summary**

Application No.

10/662,969

Examiner

Li Liu

Applicant(s)

MACDOUGALL ET AL.

Art Unit

2613

-- The MAILING DATE of this communication appears on the cover sheet with the correspondence address --

**Period for Reply**

A SHORTENED STATUTORY PERIOD FOR REPLY IS SET TO EXPIRE 3 MONTH(S) OR THIRTY (30) DAYS, WHICHEVER IS LONGER, FROM THE MAILING DATE OF THIS COMMUNICATION.

- Extensions of time may be available under the provisions of 37 CFR 1.136(a). In no event, however, may a reply be timely filed after SIX (6) MONTHS from the mailing date of this communication.
- If NO period for reply is specified above, the maximum statutory period will apply and will expire SIX (6) MONTHS from the mailing date of this communication.
- Failure to reply within the set or extended period for reply will, by statute, cause the application to become ABANDONED (35 U.S.C. § 133).
- Any reply received by the Office later than three months after the mailing date of this communication, even if timely filed, may reduce any earned patent term adjustment. See 37 CFR 1.704(b).

**Status**

- 1) ☒ Responsive to communication(s) filed on 20 November 2007.
- 2a) ☐ This action is **FINAL**. 2b) ☒ This action is non-final.
- 3) ☐ Since this application is in condition for allowance except for formal matters, prosecution as to the merits is closed in accordance with the practice under *Ex parte Quayle*, 1935 C.D. 11, 453 O.G. 213.

**Disposition of Claims**

- 4) ☒ Claim(s) 1,2,6,8-12,14,16-22,26,29 and 30 is/are pending in the application.
- 4a) Of the above claim(s) \_\_\_\_\_ is/are withdrawn from consideration.
- 5) ☐ Claim(s) \_\_\_\_\_ is/are allowed.
- 6) ☒ Claim(s) 1,2,6,8-12,14,16-22,26,29 and 30 is/are rejected.
- 7) ☐ Claim(s) \_\_\_\_\_ is/are objected to.
- 8) ☐ Claim(s) \_\_\_\_\_ are subject to restriction and/or election requirement.

**Application Papers**

- 9) ☐ The specification is objected to by the Examiner.
- 10) ☒ The drawing(s) filed on 15 September 2003 is/are: a) ☒ accepted or b) ☐ objected to by the Examiner.  
Applicant may not request that any objection to the drawing(s) be held in abeyance. See 37 CFR 1.85(a).  
Replacement drawing sheet(s) including the correction is required if the drawing(s) is objected to. See 37 CFR 1.121(d).
- 11) ☐ The oath or declaration is objected to by the Examiner. Note the attached Office Action or form PTO-152.

**Priority under 35 U.S.C. § 119**

- 12) ☐ Acknowledgment is made of a claim for foreign priority under 35 U.S.C. § 119(a)-(d) or (f).
- a) ☐ All b) ☐ Some \* c) ☐ None of:
- ☐ Certified copies of the priority documents have been received.
  - ☐ Certified copies of the priority documents have been received in Application No. \_\_\_\_\_.
  - ☐ Copies of the certified copies of the priority documents have been received in this National Stage application from the International Bureau (PCT Rule 17.2(a)).

\* See the attached detailed Office action for a list of the certified copies not received.

**Attachment(s)**

- ☒ Notice of References Cited (PTO-892)
- ☐ Notice of Draftsperson's Patent Drawing Review (PTO-948)
- ☐ Information Disclosure Statement(s) (PTO/SB/08)  
Paper No(s)/Mail Date \_\_\_\_\_
- ☐ Interview Summary (PTO-413)  
Paper No(s)/Mail Date: \_\_\_\_\_
- ☐ Notice of Informal Patent Application
- ☐ Other: \_\_\_\_\_

## **DETAILED ACTION**

### ***Continued Examination Under 37 CFR 1.114***

1. A request for continued examination under 37 CFR 1.114, including the fee set forth in 37 CFR 1.17(e), was filed in this application after final rejection. Since this application is eligible for continued examination under 37 CFR 1.114, and the fee set forth in 37 CFR 1.17(e) has been timely paid, the finality of the previous Office action has been withdrawn pursuant to 37 CFR 1.114. Applicant's submission filed on 11/16/2007 and 11/20/2007 has been entered.

### ***Response to Arguments***

2. Applicant's arguments with respect to claims 1, 2, 6, 8-12, 14, 16-22, 26, 29 and 30 have been considered but are moot in view of the new ground(s) of rejection.

### ***Claim Rejections - 35 USC § 103***

3. The following is a quotation of 35 U.S.C. 103(a) which forms the basis for all obviousness rejections set forth in this Office action:

(a) A patent may not be obtained though the invention is not identically disclosed or described as set forth in section 102 of this title, if the differences between the subject matter sought to be patented and the prior art are such that the subject matter as a whole would have been obvious at the time the invention was made to a person having ordinary skill in the art to which said subject matter pertains. Patentability shall not be negated by the manner in which the invention was made.

4. Claims 1, 6, 8-11, 14, 18-21, 29 and 30 are rejected under 35 U.S.C. 103(a) as being unpatentable over Davis (US 6,346,702) in view of Wang et al (Wang et al: "Analysis and Suppression of Continuous Periodic Interference for On-Line PD Monitoring of Power Transformers", High Voltage Engineering Symposium, 22-27

August 1999, 5.212.P5) and Lo et al (US 6,207,961) and Lochmann et al (US 4,475,038).

1). With regard to claims 1, 6, 29 and 30, Davis discloses an optical system (Figure 2B) comprising:

a source (BROADBAND SOURCE 12 in Figure 2B) for producing optical signals;  
an optical waveguide (Form the coupler 14 to FBG 18 in Figure 2B) having a noise producing element (connectors, splicers or imperfections in the FBG itself, column 1 line 40-41) and an optical filter element (the FBG 16 or 18 in Figure 2B);

a receiver for (20 in Figure 2B) converting applied optical signals into electrical signals;

a coupler (14 in Figure 2B) for coupling said produced optical signals into said optical waveguide and for coupling reflections from said noise producing element and from said optical filter element to said receiver (20 in Figure 2B) as applied optical signals (column 3 line 59-64); and

a noise reduction system (the combination of 32 and 34 in Figure 2B) for producing a frequency spectrum of the electrical signals (after the optical detection unit 20, the optical signal is converted into electrical signal, column 4 line 3-8; and as shown in the Figures 3A, 3B, 4A and 4B, the noise reduction system produces and processes frequency spectrum of the electrical signal; 34 in Figure 2B is a spectral analysis device) and removing noise produced by said noise producing element from said electrical signals (column 4 line 16-67, and a variable threshold is used to remove the background noise).

In the system of Davis et al, since the optical connectors and splices etc are present in the sensor system, the periodic noise is inherently in the noise background; and the noise reduction system of Davis removes the background noise including the periodic noise.

But, Davis et al does not expressly state (A) wherein the noise reduction system performs a frequency analysis of the electrical signals to identify a periodic noise, from said noise producing element, which is removed from the electrical signals using frequency based gating of the frequency spectrum; (B) the frequency analysis is a Fourier analysis (claim 6); (C) wherein the frequency based gating comprises of selecting a bandwidth where periodic noise has been identified and removing the bandwidth from the electrical signals (claim 29); and (D) wherein the noise reduction system identifies periodic noise by identifying a rapidly varying signal from the frequency analysis (claim 30).

Performing a frequency analysis, such as a Fourier analysis, to identify periodic noise or other kinds of noise component from the frequency analysis on an electrical signal and the frequency based gating are well known and widely used method in the art. Wang et al discloses a system and method that uses Fast Fourier Transform technique to analyze the periodic noise of an electrical signal, the noise reduction system performs a frequency analysis of the electrical signals to identify a periodic noise, from said noise producing element, which is removed from the electrical signals using frequency based gating of the frequency spectrum (Abstract, Figures 2 and 3, Methods of Interference Eliminated); and the frequency analysis is a Fourier analysis

(ABSTRACT, FFT technique); wherein the frequency based gating comprises of selecting a bandwidth where periodic noise has been identified and removing the bandwidth from the electrical signals (Digital Filtering Technique, FFT Threshold Digital Filter and Multi-Band-Pass Digital Filter, a multi-band rejection digital filter is used to remove the noise components); and wherein the noise reduction system identifies periodic noise by identifying a rapidly varying signal from the frequency analysis (Figures 2 and 3, and Digital Filtering Technique).

Another prior art, Lochmann et al, also teaches a Fourier analysis to remove or filter high frequency noise from raw spectral data to obtain a "smooth data curve". Lochmann et al teaches a three steps procedure: first, the data is transformed by Fourier analysis into a sinusoidal representation; the second step of the filtering procedure is the application of a damping factor to the transformed data; the third step of the filtering procedure involves transforming the damped data back into numerical form by inverse Fourier analysis (Figure 7, column 8 line 48 to column9 line 36). Lochmann et al teaches that Fourier analysis of the raw data has the effect of isolating the high-frequency noise relative to the data signal; by damping the transformed data and inversely transforming it back into a numerical representation, the high-frequency noise is eliminated without substantially affecting the data signal.

Although Wang et al teaches suppression of the periodic interference for partial discharged monitoring of power transform and Lochmann et al teaches removing of high frequency noise so to enhance neutron induced gamma ray logging records, both references are reasonably pertinent to the particular problem with which the applicant

was concerned; that is, remove noise frequency component from electrical signals: obtaining electrical signal, using frequency analysis or fast Fourier transform technique to identify the noise frequency component, and removing the noise component, so to improve the signal quality or signal to noise ratio.

Another prior art, Lo et al, also teaches a fiber-optic optical sensor and uses FFT to remove noise frequencies. Lo et al teaches that the SNR of the sensor was improved through the use of digital signal averaging and FFT filters; the noise frequencies were efficiently removed by selecting a pass band in the power spectrum before transformation back to the time domain using inverse FFT (column 4, line 34-43).

Both Lochmann et al and Lo et al teach that the FFT is particularly preferred because of the availability of the fast fourier and inverse fast fourier computer subroutines at low cost and high speed (column 9 line 45-53 of Lochmann, and column 4 line 41-48 of Lo et al). Therefore, it would have been obvious to one of ordinary skill in the art at the time the invention was made to apply the frequency analysis and noise gating as taught by Wang et al and Lochmann et al and Lo et al to the system of Davis et al so that the noise can be efficiently identified and removed or gated out of the electrical signals in frequency domain, and measurement accuracy can be enhanced.

2). With regard to claim 8, Davis et al and Wang et al and Lochmann et al and Lo et al disclose all of the subject matter as applied to claim 1 above. And Davis et al further discloses wherein the optical filter element includes a fiber Bragg grating (FBG 16 or 18 in Figure 1B).

3). With regard to claim 9, Davis et al and Wang et al and Lochmann et al and Lo et al disclose all of the subject matter as applied to claim 1 above. And Davis further discloses wherein the optical waveguide includes a discontinuity (connectors, splicers or imperfections in the FBG itself, column 1 line 40-41).

4). With regard to claim 10, Davis et al and Wang et al and Lochmann et al and Lo et al disclose all of the subject matter as applied to claim 1 above. And Davis further discloses wherein the discontinuity is a splice (splicers, column 1 line 40-41).

5). With regard to claims 11, 14 and 26, Davis discloses a sensor comprising:  
a source for producing optical signals (BROADBAND SOURCE 12 in Figure 2B);  
an optical waveguide (Form the coupler 14 to FBG 18 in Figure 2B) having a noise producing element (connectors, splicers or imperfections in the FBG itself, column 1 line 40-41) and an optical filter element (the FBG 16 or 18 in Figure 2B);

a receiver (20 in Figure 2B) for converting applied optical signals into amplified electrical signals;

a coupler (14 in Figure 2B) for coupling said produced optical signals into said optical waveguide and for coupling reflections from said optical waveguide as applied optical signals to said receiver (column 3 line 59-64); and

a signal processor (the combination of 32 and 34 in Figure 2B) for producing a frequency spectrum of the electrical signals (after the optical detection unit 20, the optical signal is converted into electrical signal, column 4 line 3-8; and as shown in the Figures 3A, 3B, 4A and 4B, the signal processor produces and processes frequency spectrum of the electrical signal; 34 in Figure 2B is a spectral analysis device) and



removing noise produced by said noise producing element from said electrical signals (column 4 line 16-67, and a variable threshold is used to remove the background noise).

In the system of Davis et al, since the optical connectors and splices etc are present in the sensor system, the periodic noise is inherently in the noise background; and the noise reduction system of Davis removes the background noise including the periodic noise.

But, Davis et al does not expressly state (A) wherein the signal processor performs a frequency analysis of the electrical signals to identify and remove a periodic noise, from the noise producing element, which is removed from the electrical signals using frequency based gating of the frequency spectrum; (B) wherein the frequency analysis is a Fourier analysis (claim 14); and (C) wherein the signal processor identifies periodic noise by identifying a rapidly varying signal from the frequency analysis (claim 26).

Performing a frequency analysis, such as a Fourier analysis, to identify periodic noise or other kinds of noise component from the frequency analysis on an electrical signal and the frequency based gating are well known and widely used method in the art. Wang et al discloses a system and method that uses Fast Fourier Transform technique to analyze the periodic noise of an electrical signal, the noise reduction system performs a frequency analysis of the electrical signals to identify a periodic noise, from said noise producing element, which is removed from the electrical signals using frequency based gating of the frequency spectrum (Abstract, Figures 2 and 3, Methods of Interference Eliminated); and the frequency analysis is a Fourier analysis

(ABSTRACT, FFT technique); wherein the frequency based gating comprises of selecting a bandwidth where periodic noise has been identified and removing the bandwidth from the electrical signals (Digital Filtering Technique, FFT Threshold Digital Filter and Multi-Band-Pass Digital Filter, a multi-band rejection digital filter is used to remove the noise components); and wherein the noise reduction system identifies periodic noise by identifying a rapidly varying signal from the frequency analysis (Figures 2 and 3, and Digital Filtering Technique).

Another prior art, Lochmann et al, also teaches a Fourier analysis to remove or filter high frequency noise from raw spectral data to obtain a "smooth data curve".

Lochmann et al teaches a three steps procedure: first, the data is transformed by Fourier analysis into a sinusoidal representation; the second step of the filtering procedure is the application of a damping factor to the transformed data; the third step of the filtering procedure involves transforming the damped data back into numerical form by inverse Fourier analysis (Figure 7, column 8 line 48 to column9 line 36).

Lochmann et al teaches that Fourier analysis of the raw data has the effect of isolating the high-frequency noise relative to the data signal; by damping the transformed data and inversely transforming it back into a numerical representation, the high-frequency noise is eliminated without substantially affecting the data signal.

Although Wang et al teaches suppression of the periodic interference for partial discharged monitoring of power transform and Lochmann et al teaches removing of high frequency noise so to enhance neutron induced gamma ray logging records, both references are reasonably pertinent to the particular problem with which the applicant

was concerned; that is, remove noise frequency component from electrical signals: obtaining electrical signal, using frequency analysis or fast Fourier transform technique to identify the noise frequency component, and removing the noise component, so to improve the signal quality or signal to noise ratio.

Another prior art, Lo et al, also teaches a fiber-optic optical sensor and uses FFT to remove noise frequencies. Lo et al teaches that the SNR of the sensor was improved through the use of digital signal averaging and FFT filters; the noise frequencies were efficiently removed by selecting a pass band in the power spectrum before transformation back to the time domain using inverse FFT (column 4, line 34-43).

Both Lochmann et al and Lo et al teach that the FFT is particularly preferred because of the availability of the fast fourier and inverse fast fourier computer subroutines at low cost and high speed (column 9 line 45-53 of Lochmann, and column 4 line 41-48 of Lo et al). Therefore, it would have been obvious to one of ordinary skill in the art at the time the invention was made to apply the frequency analysis and noise gating as taught by Wang et al and Lochmann et al and Lo et al to the system of Davis et al so that the noise can be efficiently identified and removed or gated out of the electrical signals in frequency domain, and measurement accuracy can be enhanced.

6). With regard to claim 18, Davis et al and Wang et al and Lochmann et al and Lo et al disclose all of the subject matter as applied to claim 11 above. And Davis et al further discloses wherein the optical filter element includes a fiber Bragg grating (FBG 16 or 18 in Figure 1B).

7). With regard to claim 19, Davis et al and Wang et al and Lochmann et al and Lo et al disclose all of the subject matter as applied to claim 11 above. And Davis et al further discloses wherein the optical waveguide includes a discontinuity (connectors, splicers or imperfections in the FBG itself, column 1 line 40-41).

8). With regard to claim 20, Davis et al and Wang et al and Lochmann et al and Lo et al disclose all of the subject matter as applied to claim 1 above. And Davis et al further discloses wherein the discontinuity is a splice (splicers, column 1 line 40-41).

9). With regard to claim 21, Davis discloses a method of compensating for optical reflection comprising:

producing an optical signal (BROADBAND SOURCE 12 in Figure 2B);

coupling (14 in Figure 2B) the optical signal into an optical waveguide having a noise producing element (e.g., splicer and connectors) and an optical filter element (the FBG in Figure 2B);

converting (20 in Figure 2B) reflections along the optical waveguide into electrical signals; and

removing noise (the combination of 32 and 34 in Figure 2B) produced by the noise producing element from the electrical signals such that the electrical signals from the optical filter element are retained (column 4 line 16-67).

Davis uses spectral analysis to analyze the noise (32 and 34 in Figure 2B, and Figure 3 and 4) and a variable threshold is used to remove the background noise; and removing noise includes performing a frequency analysis (34 in Figure 2B is the spectral analysis device). In the system of Davis et al, since the optical connectors and

splices etc are present in the sensor system, the periodic noise is inherently in the noise background; and the noise reduction system of Davis removes the background noise including the periodic noise.

But Davis does not expressly disclose wherein gating out the periodic noise produced by the noise producing element from the electrical signals includes producing a frequency spectrum of the electrical signals and using frequency based gating to remove a first signal varying rapidly relative to a second signal as determined by a frequency analysis of the frequency spectrum.

Performing a frequency analysis, such as a Fourier analysis, to identify periodic noise or other kinds of noise component from the frequency analysis on an electrical signal and the frequency based gating are well known and widely used method in the art. Wang et al discloses a method that uses Fast Fourier Transform technique to analyze the periodic noise of an electrical signal, the noise reduction system performs a frequency analysis of the electrical signals to identify a periodic noise (the first signal varying rapidly relative to a second signal that is the signal shown in Figure 3d), which is removed from the electrical signals using frequency based gating of the frequency spectrum (Abstract, Figures 2 and 3, Methods of Interference Eliminated); wherein the frequency based gating comprises of selecting a bandwidth where periodic noise has been identified and removing the bandwidth from the electrical signals (Digital Filtering Technique, FFT Threshold Digital Filter and Multi-Band-Pass Digital Filter, a multi-band rejection digital filter is used to remove the noise components); and the method produces a frequency spectrum of the electrical signals (Figure 2) and uses frequency

based gating to remove a first signal varying rapidly relative to a second signal as determined by a frequency analysis of the frequency spectrum (Figures 2 and 3, and Digital Filtering Technique).

Another prior art, Lochmann et al, also teaches a Fourier analysis to remove or filter high frequency noise ("the first signal varying rapidly") from raw spectral data to obtain a "smooth data curve" (the "second signal" or the required data signal).

Lochmann et al teaches a three steps procedure: first, the data is transformed by Fourier analysis into a sinusoidal representation; the second step of the filtering procedure is the application of a damping factor to the transformed data; the third step of the filtering procedure involves transforming the damped data back into numerical form by inverse Fourier analysis (Figure 7, column 8 line 48 to column 9 line 36).

Lochmann et al teaches that Fourier analysis of the raw data has the effect of isolating the high-frequency noise relative to the data signal; by damping the transformed data and inversely transforming it back into a numerical representation, the high-frequency noise is eliminated without substantially affecting the data signal.

Although Wang et al teaches suppression of the periodic interference for partial discharged monitoring of power transform and Lochmann et al teaches removing of high frequency noise so to enhance neutron induced gamma ray logging records, both references are reasonably pertinent to the particular problem with which the applicant was concerned; that is, remove noise frequency component from electrical signals: obtaining electrical signal, using frequency analysis or fast Fourier transform technique

to identify the noise frequency component, and removing the noise component, so to improve the signal quality or signal to noise ratio.

Another prior art, Lo et al, also teaches a fiber-optic optical sensor and uses FFT to remove noise frequencies. Lo et al teaches that the SNR of the sensor was improved through the use of digital signal averaging and FFT filters; the noise frequencies (the first signal varying rapidly relative to a second signal that is the fluorescence signal) were efficiently removed by selecting a pass band in the power spectrum before transformation back to the time domain using inverse FFT (column 4, line 34-43).

Both Lochmann et al and Lo et al teach that the FFT is particularly preferred because of the availability of the fast fourier and inverse fast fourier computer subroutines at low cost and high speed (column 9 line 45-53 of Lochmann, and column 4 line 41-48 of Lo et al), and the SNR of the signal is improved. Therefore, it would have been obvious to one of ordinary skill in the art at the time the invention was made to apply the frequency analysis and noise gating as taught by Wang et al and Lochmann et al and Lo et al to the system of Davis et al so that the noise can be efficiently identified and removed or gated out of the electrical signals in frequency domain, and measurement accuracy can be enhanced.

5. Claims 2, 12 and 22 are rejected under 35 U.S.C. 103(a) as being unpatentable over Davis et al and Wang et al and Lochmann et al and Lo et al as applied to claims 1, 11 and 21 above, and in further view of Keown (US 4,143,350).

Davis et al and Wang et al and Lochmann et al and Lo et al as discloses all of the subject matter as applied to claims 1, 11 and 21 above. And Davis teaches that the

"variable threshold peak detection unit 32 determines the DC component of the background signal by performing two running averages along the spectral trace. ...

The local threshold value includes an overall minimum level term which is comparable to the noise level of the variable threshold peak detection unit 32". But Davis does not explicitly state wherein the noise reduction system or signal processor averages broadband noise and then subtracts the averaged level from the electrical signals.

However, the method of averaging the broadband noise and then subtracting the averaged level from the electrical signals is a well known method and widely used in the signal processing. As disclosed by Lo et al, the SNR of the sensor is improved through the use of digital averaging (column 4, line 34-35, Figure 6). Lochmann et al also teaches to subtract the background "baseline" to get the "true" signal component.

Another prior art, Keown, teaches to average the broadband noise and then subtract the averaged level from the electrical signals (ABSTRACT and column 6, line 6-15).

Therefore, it would have been obvious to one of ordinary skill in the art at the time the invention was made to apply the method of averaging noise taught by Lo and Lochmann and Keown to the system of Davis et al and Wang et al so that the broadband noise can be effectively suppressed and system performance is enhanced.

6. Claims 16 and 17 are rejected under 35 U.S.C. 103(a) as being unpatentable over Davis et al and Wang et al and Lochmann et al and Lo et al as applied to claim 11 above, and in further view of Kringlebotn (US 6,097,487).



Davis et al discloses all of the subject matter as applied to claim 11 above. And Davis et al discloses a broadband source. Davis also discloses that the broadband source includes a narrow source swept over a broad band (column 3, line 53-55). But Davis does not expressly disclose that the source includes a tunable laser (claim 16); and the source includes a broadband light source and a tunable filter (claim 17).

However, Kringlebotn et al, in the same field endeavor, discloses a tunable laser or a broadband light source and a tunable filter (1 and 2 in Figure 1, Figure 4 and 6, column 2 line 62-67). By using a tunable filter, a fixed F-P filter, and a reference wavelength FBG, Kringlebotn et al constructs either a spectrum analyzer with a high degree of wavelength accuracy, or a control system for a tunable laser or a multi-wavelength laser array to be able to control and set the wavelength of the tunable laser/wavelengths of the laser array with a high degree of repeatability and accuracy, typically <1 pm.

Therefore, it would have been obvious to one of ordinary skill in the art at the time the invention was made to apply a tunable laser or a broadband light source with a tunable filter taught by Kringlebotn et al to the system of Davis et al so that an accurate frequency/wavelength scale can be obtained and system performance can be enhanced.

### ***Conclusion***

7. The prior art made of record and not relied upon is considered pertinent to applicant's disclosure.

Mathews (US 5,431,170) teaches a device using the FFT to remove the noise components in the signal from the infra red sensor.

8. Any inquiry concerning this communication or earlier communications from the examiner should be directed to Li Liu whose telephone number is (571)270-1084. The examiner can normally be reached on Mon-Fri, 8:00 am - 5:30 pm, alternating Fri off.

If attempts to reach the examiner by telephone are unsuccessful, the examiner's supervisor, Ken Vanderpuye can be reached on (571)272-3078. The fax phone number for the organization where this application or proceeding is assigned is 571-273-8300.

Information regarding the status of an application may be obtained from the Patent Application Information Retrieval (PAIR) system. Status information for published applications may be obtained from either Private PAIR or Public PAIR. Status information for unpublished applications is available through Private PAIR only. For more information about the PAIR system, see <http://pair-direct.uspto.gov>. Should you have questions on access to the Private PAIR system, contact the Electronic Business Center (EBC) at 866-217-9197 (toll-free). If you would like assistance from a USPTO Customer Service Representative or access to the automated information system, call 800-786-9199 (IN USA OR CANADA) or 571-272-1000.

Li Liu  
February 03, 2008

  
KENNETH VANDERPUYE  
SUPERVISORY PATENT EXAMINER